

# Hansen's basic RBC model

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## 1 Hansen's RBC model

Hansen's RBC model

- First RBC model was Kydland and Prescott
  - (1982) "Time to build and aggregate fluctuations," *Econometrica*
  - Complicated
    - \* lagged cumulative investment
    - \* strange utility function
    - \* Lots added to look for persistence
- Hansen's model much simpler
  - (1985) "Indivisible labor and the business cycle," *Journal of Monetary Economics*
  - Simple
  - Added indivisible labor to gain persistence and covariance with output
  - Set rules for RBC game
    - \* Match second moments
    - \* Newer rule: match impulse response functions

Hansen's basic model

- Robinson Crusoe maximizes the discounted utility function

$$\max \sum_{t=0}^{\infty} \beta^t u(c_t, l_t)$$

- The specific utility functions

$$u(c_t, 1 - h_t) = \ln c_t + A \ln(1 - h_t)$$

with  $A > 0$ .

- The production function is

$$f(\lambda_t, k_t, h_t) = \lambda_t k_t^\theta h_t^{1-\theta}$$

- $\lambda_t$  is a random technology variable that follows the process

$$\lambda_{t+1} = \gamma \lambda_t + \varepsilon_{t+1}$$

for  $0 < \gamma < 1$ .  $\varepsilon_t$  iid, positive, bounded above,  $E\varepsilon_t = 1 - \gamma$ .

–  $\implies E \lambda_t$  is 1 and  $\lambda_{t+1} > 0$ .

Hansen's basic model (continued)

- Capital accumulation follows the process

$$k_{t+1} = (1 - \delta)k_t + i_t$$

- The feasibility constraint is

$$f(\lambda_t, k_t, h_t) \geq c_t + i_t$$

Bellmans equation

The basic Bellmans equation

$$V(k_t, \lambda_t) = \max_{c_t, h_t} [\ln c_t + A \ln(1 - h_t) + \beta E_t [V(k_{t+1}, \lambda_{t+1}) \mid \lambda_t]]$$

subject to

$$\begin{aligned} \lambda_t k_t^\theta h_t^{1-\theta} &\geq c_t + i_t, \\ \lambda_{t+1} &= \gamma \lambda_t + \varepsilon_{t+1}, \text{ and} \\ k_{t+1} &= (1 - \delta)k_t + i_t. \end{aligned}$$

Simpler to write as

$$\begin{aligned} V(k_t, \lambda_t) &= \max_{k_{t+1}, h_t} [\ln (\lambda_t k_t^\theta h_t^{1-\theta} + (1 - \delta)k_t - k_{t+1}) \\ &\quad + A \ln(1 - h_t) + \beta E_t [V(k_{t+1}, \lambda_{t+1}) \mid \lambda_t]] \end{aligned}$$

$k_{t+1}$  and  $h_t$  are control variables

First order conditions

- First order conditions are

$$\frac{\partial V(k_t, \lambda_t)}{\partial k_{t+1}} = 0 = -\frac{1}{\lambda_t k_t^\theta h_t^{1-\theta} + (1-\delta)k_t - k_{t+1}} + \beta E_t [V_k(k_{t+1}, \lambda_{t+1}) \mid \lambda_t]$$

and

$$\frac{\partial V(k_t, \lambda_t)}{\partial h_t} = 0 = (1-\theta) \frac{1}{\lambda_t k_t^\theta h_t^{1-\theta} + (1-\delta)k_t - k_{t+1}} (\lambda_t k_t^\theta h_t^{-\theta}) - A \frac{1}{1-h_t}$$

- The Benveniste-Scheinkman envelope theorem condition is

$$\frac{\partial V(k_t, \lambda_t)}{\partial k_t} = \frac{1}{\lambda_t k_t^\theta h_t^{1-\theta} + (1-\delta)k_t - k_{t+1}} (\theta \lambda_t k_t^{\theta-1} h_t^{1-\theta} + (1-\delta))$$

Simplifying the first order conditions

- First order conditions can be written as

$$\frac{1}{\lambda_t k_t^\theta h_t^{1-\theta} + (1-\delta)k_t - k_{t+1}} = \beta E_t \left[ \frac{\theta \lambda_{t+1} k_{t+1}^{\theta-1} h_{t+1}^{1-\theta} + (1-\delta)}{\lambda_{t+1} k_{t+1}^\theta h_{t+1}^{1-\theta} + (1-\delta)k_{t+1} - k_{t+2}} \mid \lambda_t \right]$$

and

$$(1-\theta)(1-h_t)(\lambda_t k_t^\theta h_t^{-\theta}) = A(\lambda_t k_t^\theta h_t^{1-\theta} + (1-\delta)k_t - k_{t+1})$$

- In equilibrium,

$$c_t = \lambda_t k_t^\theta h_t^{1-\theta} + (1-\delta)k_t - k_{t+1}$$

Simplifying the first order conditions (continued)

Factor markets give

$$r_t = \theta \lambda_t k_t^{\theta-1} h_t^{1-\theta}$$

and

$$w_t = (1-\theta) \lambda_t k_t^\theta h_t^{-\theta}$$

First order conditions are simply

$$\frac{1}{c_t} = \beta E_t \left[ \frac{r_{t+1} + (1-\delta)}{c_{t+1}} \mid \lambda_t \right]$$

and

$$(1-h_t)w_t = A c_t$$

Stationary states

- Stationary state value of  $\bar{h} = h_t = h_{t+1}$  is

$$\bar{h} = \frac{1}{1 + \frac{A}{(1-\theta)} \left[ 1 - \frac{\beta\delta\theta}{1-\beta(1-\delta)} \right]},$$

- Stationary state value of  $\bar{k} = k_t = k_{t+1} = k_{t+2}$  is

$$\bar{k} = \bar{h} \left[ \frac{\theta\bar{\lambda}}{\frac{1}{\beta} - (1-\delta)} \right]^{\frac{1}{1-\theta}}.$$

How to study dynamics

1. Find the approximate Value function and Plan
  - (a) These will describe the dynamics within the precision of the approximation
  - (b) Can be complicated to find
    - i. Especially if the domain of stochastic variable is large
  - (c) Can be impossible
    - i. If the model is not single agent
    - ii. If the model can not be approximated by social planner
2. Alternative approaches
  - (a) Log linear approximation of the model
    - i. After the optimization has been done
    - ii. After equilibrium conditions have been imposed
  - (b) Quadratic linear approximation of the problem

Log-linearization techniques

- Consider a function of the form

$$F(x_t) = \frac{G(x_t)}{H(x_t)}$$

- Taking logs of both side gives

$$\ln(F(x_t)) = \ln(G(x_t)) - \ln(H(x_t))$$

- The first order Taylor series expansion
  - around the stationary state values  $\bar{x}$

– gives

$$\begin{aligned}\ln(F(\bar{x})) + \frac{F'(\bar{x})}{F(\bar{x})}(x_t - \bar{x}) &\approx \ln(G(\bar{x})) + \frac{G'(\bar{x})}{G(\bar{x})}(x_t - \bar{x}) \\ &\quad - \ln(H(\bar{x})) - \frac{H'(\bar{x})}{H(\bar{x})}(x_t - \bar{x})\end{aligned}$$

Log-linearization techniques (direct method)

- In the stationary state

$$\ln(F(\bar{x})) = \ln(G(\bar{x})) - \ln(H(\bar{x}))$$

- So the first order Taylor expansion can be written as

$$\frac{F'(\bar{x})}{F(\bar{x})}(x_t - \bar{x}) \approx \frac{G'(\bar{x})}{G(\bar{x})}(x_t - \bar{x}) - \frac{H'(\bar{x})}{H(\bar{x})}(x_t - \bar{x})$$

- Remember that this holds only near  $\bar{x}$

An example using a Cobb-Douglas production function

$$Y_t = \lambda_t K_t^\theta H_t^{1-\theta}$$

- Take logs

$$\ln Y_t = \ln \lambda_t + \theta \ln K_t + (1 - \theta) \ln H_t$$

- first order Taylor expansion gives

$$\begin{aligned}\ln \bar{Y} + \frac{1}{\bar{Y}}(Y_t - \bar{Y}) &\approx \ln \bar{\lambda} + \frac{1}{\bar{\lambda}}(\lambda_t - \bar{\lambda}) + \theta \ln \bar{K} + \frac{\theta}{\bar{K}}(K_t - \bar{K}) \\ &\quad + (1 - \theta) \ln \bar{H} + \frac{(1 - \theta)}{\bar{H}}(H_t - \bar{H})\end{aligned}$$

- Since in a stationary state

$$\ln \bar{Y} = \ln \bar{\lambda} + \theta \ln \bar{K} + (1 - \theta) \ln \bar{H}$$

- get

$$\frac{1}{\bar{Y}}(Y_t - \bar{Y}) \approx \frac{1}{\bar{\lambda}}(\lambda_t - \bar{\lambda}) + \frac{\theta}{\bar{K}}(K_t - \bar{K}) + \frac{(1 - \theta)}{\bar{H}}(H_t - \bar{H})$$

- That reduces to

$$\frac{Y_t}{\bar{Y}} + 1 \approx \frac{\lambda_t}{\bar{\lambda}} + \frac{\theta K_t}{\bar{K}} + \frac{(1 - \theta) H_t}{\bar{H}}$$

Log-linearization techniques (Uhlig's method)

- Write the original variable as

$$X_t = \bar{X} e^{\tilde{X}_t}$$

or

$$\tilde{X}_t = \ln X_t - \ln \bar{X}$$

- bring together all the exponential terms that you can

$$\frac{A_t B_t^\alpha}{C_t^\delta} = \frac{\bar{A} \bar{A}^{\tilde{A}_t} \bar{B}^\alpha e^{\alpha \tilde{B}_t}}{\bar{C}^\delta e^{\delta \tilde{C}_t}}$$

becomes

$$\frac{\bar{A} \bar{B}^\alpha}{\bar{C}^\delta} e^{\tilde{A}_t + \alpha \tilde{B}_t - \delta \tilde{C}_t}$$

Reference: Uhlig, Harald, (1999) "A toolkit for analysing nonlinear dynamic stochastic models easily", in Ramon Marimon and Andrew Scott, Eds., Computational Methods for the Study of Dynamic Economies, Oxford University Press, Oxford, p.30-61.

Log-linearization techniques (Uhlig's method)

- The Taylor series expansion (linear) gives

$$\begin{aligned} e^{\tilde{A}_t + \alpha \tilde{B}_t - \delta \tilde{C}_t} &\approx e^{\tilde{A}_t + \alpha \tilde{B}_t - \delta \tilde{C}_t} + e^{\tilde{A}_t + \alpha \tilde{B}_t - \delta \tilde{C}_t} (\tilde{A}_t - \tilde{A}) \\ &\quad + \alpha e^{\tilde{A}_t + \alpha \tilde{B}_t - \delta \tilde{C}_t} (\tilde{B}_t - \tilde{B}) - \delta e^{\tilde{A}_t + \alpha \tilde{B}_t - \delta \tilde{C}_t} (\tilde{C}_t - \tilde{C}) \\ &= 1 + \tilde{A}_t + \alpha \tilde{B}_t - \delta \tilde{C}_t, \end{aligned}$$

- So

$$e^{\tilde{A}_t + \alpha \tilde{B}_t - \delta \tilde{C}_t} \approx 1 + \tilde{A}_t + \alpha \tilde{B}_t - \delta \tilde{C}_t$$

- The approximation is

$$\frac{A_t B_t^\alpha}{C_t^\delta} \approx \frac{\bar{A} \bar{B}^\alpha}{\bar{C}^\delta} (1 + \tilde{A}_t + \alpha \tilde{B}_t - \delta \tilde{C}_t)$$

Log-linearization techniques (Uhlig's method)

- Some rules from Uhlig

$$\begin{aligned} e^{\tilde{X}_t + a \tilde{Y}_t} &\approx 1 + \tilde{X}_t + a \tilde{Y}_t, \\ \tilde{X}_t \tilde{Y}_t &\approx 0, \\ E_t [a e^{\tilde{X}_{t+1}}] &\approx a + a E_t [\tilde{X}_{t+1}] \\ E_t [X_{t+1}] &= \bar{X} (1 + E_t [\tilde{X}_{t+1}]) \end{aligned}$$

Log linear version of Hansen's model

- The five equations of the Hansen model are (adjusted)

$$\begin{aligned}
1 &= \beta E_t \left[ \frac{C_t}{C_{t+1}} (r_{t+1} + (1 - \delta)) \right] \\
AC_t &= (1 - \theta) (1 - H_t) \frac{Y_t}{H_t} \\
C_t &= Y_t + (1 - \delta)K_t - K_{t+1} \\
Y_t &= \lambda_t K_t^\theta H_t^{1-\theta} \\
r_t &= \theta \frac{Y_t}{K_t}
\end{aligned}$$

- We will do the log-linearization equation by equation

Log linear version of Hansen's model

- First equation

$$\begin{aligned}
1 &= \beta E_t \left[ \frac{C_t}{C_{t+1}} (r_{t+1} + (1 - \delta)) \right] \\
1 &= \beta E_t \left[ \frac{\bar{C} e^{\tilde{C}_t}}{\bar{C} e^{\tilde{C}_{t+1}}} \bar{r} e^{\tilde{r}_{t+1}} + (1 - \delta) \frac{\bar{C} e^{\tilde{C}_t}}{\bar{C} e^{\tilde{C}_{t+1}}} \right] \\
&= \beta E_t \left[ \bar{r} e^{\tilde{C}_t - \tilde{C}_{t+1} + \tilde{r}_{t+1}} + (1 - \delta) e^{\tilde{C}_t - \tilde{C}_{t+1}} \right] \\
&\approx \beta \left( \bar{r} E_t \left[ 1 + \tilde{C}_t - \tilde{C}_{t+1} + \tilde{r}_{t+1} \right] + (1 - \delta) \left[ 1 + \tilde{C}_t - \tilde{C}_{t+1} \right] \right) \\
&= E_t \left[ 1 + \tilde{C}_t - \tilde{C}_{t+1} + \beta \bar{r} \tilde{r}_{t+1} \right],
\end{aligned}$$

or (after cancelling the 1's and cleaning up the expectations)

$$0 \approx \tilde{C}_t - E_t \tilde{C}_{t+1} + \beta \bar{r} E_t \tilde{r}_{t+1}$$

Log linear version of Hansen's model

- Second equation

$$\begin{aligned}
AC_t &= (1 - \theta) (1 - H_t) \frac{Y_t}{H_t} \\
A\bar{C} e^{\tilde{C}_t} &= (1 - \theta) \frac{\bar{Y}}{\bar{H}} e^{\tilde{Y}_t - \tilde{H}_t} - (1 - \theta) \bar{Y} e^{\tilde{Y}_t} \\
A\bar{C} \left( 1 + \tilde{C}_t \right) &\approx (1 - \theta) \frac{\bar{Y}}{\bar{H}} \left( 1 + \tilde{Y}_t - \tilde{H}_t \right) - (1 - \theta) \bar{Y} \left( 1 + \tilde{Y}_t \right) \\
A\bar{C} \tilde{C}_t &\approx \left[ (1 - \theta) \frac{(1 - \bar{H}) \bar{Y}}{\bar{H}} \right] \tilde{Y}_t - (1 - \theta) \frac{\bar{Y}}{\bar{H}} \tilde{H}_t
\end{aligned}$$

- given that in the stationary state

$$A\bar{C} = (1 - \theta) \frac{(1 - \bar{H})\bar{Y}}{\bar{H}}$$

Log linear version of Hansen's model

- This becomes

$$\tilde{C}_t \approx \tilde{Y}_t - \frac{(1 - \theta) \frac{\bar{Y}}{\bar{H}}}{(1 - \theta) \frac{(1 - \bar{H})\bar{Y}}{\bar{H}}} \tilde{H}_t = \tilde{Y}_t - \frac{\tilde{H}_t}{1 - \bar{H}}$$

- so

$$0 = \tilde{C}_t - \tilde{Y}_t + \frac{\tilde{H}_t}{1 - \bar{H}}$$

Log linear version of Hansen's model

- The next three equations (in their Log-linear form) are

$$0 \approx \bar{Y}\tilde{Y}_t - \bar{C}\tilde{C}_t + \bar{K} \left[ (1 - \delta)\tilde{K}_t - \tilde{K}_{t+1} \right]$$

$$0 \approx \tilde{\lambda}_t + \theta\tilde{K}_t + (1 - \theta)\tilde{H}_t - \tilde{Y}_t$$

$$0 \approx \tilde{Y}_t - \tilde{K}_t - \tilde{r}_t$$

- where  $\bar{r} = \theta\bar{Y}/\bar{K}$

Log linear version of Hansen's model

- The stochastic process is

$$\lambda_{t+1} = \gamma\lambda_t + \varepsilon_{t+1}$$

- putting in the log difference of the  $\lambda$ 's

$$\bar{\lambda}e^{\tilde{\lambda}_{t+1}} = \gamma\bar{\lambda}e^{\tilde{\lambda}_t} + \varepsilon_{t+1}$$

- the linear approximation is

$$\bar{\lambda} \left( 1 + \tilde{\lambda}_{t+1} \right) = \gamma\bar{\lambda} \left( 1 + \tilde{\lambda}_t \right) + \varepsilon_{t+1}$$

- So the simple version is

$$\tilde{\lambda}_{t+1} = \gamma\tilde{\lambda}_t + \mu_{t+1}$$

The log-linear version of the model



- The equations of the full log-linear model are

$$\begin{aligned}
0 &= \tilde{C}_t - E_t \tilde{C}_{t+1} + \beta \bar{r} E_t \tilde{r}_{t+1} \\
0 &= \tilde{C}_t - \tilde{Y}_t + \frac{\tilde{H}_t}{1 - \bar{H}} \\
0 &= \bar{Y} \tilde{Y}_t - \bar{C} \tilde{C}_t + \bar{K} \left[ (1 - \delta) \tilde{K}_t - \tilde{K}_{t+1} \right] \\
0 &= \tilde{\lambda}_t + \theta \tilde{K}_t + (1 - \theta) \tilde{H}_t - \tilde{Y}_t \\
0 &= \tilde{Y}_t - \tilde{K}_t - \tilde{r}_t
\end{aligned}$$

and

$$\tilde{\lambda}_{t+1} = \gamma \tilde{\lambda}_t + \mu_{t+1}$$

Solving the log-linear version of the model

- The variables of the model are  $\left\{ \tilde{K}_{t+1} \quad \tilde{Y}_t \quad \tilde{C}_t \quad \tilde{H}_t \quad \tilde{r}_t \right\}$  plus the stochastic variables  $\lambda_t$
- Define the state variables as

$$x_t = \left[ \tilde{K}_t \right]$$

- Define the "jump" variables as

$$y_t = \begin{bmatrix} Y_t \\ C_t \\ H_t \\ r_t \end{bmatrix}$$

- Define the stochastic variable as

$$z_t = [\lambda_t]$$

Solving the log-linear version of the model

- The model can be written as

$$\begin{aligned}
0 &= Ax_t + Bx_{t-1} + Cy_t + Dz_t, \\
0 &= E_t [Fx_{t+1} + Gx_t + Hx_{t-1} + Jy_{t+1} + Ky_t + Lz_{t+1} + Mz_t], \\
z_{t+1} &= Nz_t + \varepsilon_{t+1}, \quad E_t(\varepsilon_{t+1}) = 0.
\end{aligned}$$

Where

$$A = \begin{bmatrix} 0 \\ -K \\ 0 \\ 0 \end{bmatrix} \quad B = \begin{bmatrix} 0 \\ K(-\delta + 1) \\ \theta \\ -1 \end{bmatrix}$$

$$C = \begin{bmatrix} 1 & -1 & -\frac{1}{1-H} & 0 \\ \bar{Y} & -\bar{C} & 0 & 0 \\ -1 & 0 & 1-\theta & 0 \\ 1 & 0 & 0 & -1 \end{bmatrix}$$

Solving the linear version of the model

$$D = \begin{bmatrix} 0 \\ 0 \\ 1 \\ 0 \end{bmatrix}$$

$$F = [0], \quad G = [0], \quad H = [0],$$

$$J = [0 \quad -1 \quad 0 \quad \beta\bar{r}],$$

$$K = [0 \quad 1 \quad 0 \quad 0],$$

$$L = [0]$$

$$M = [0]$$

$$N = [\gamma]$$

Solving the linear version of the model

- We look for a solution of the form

$$x_t = Px_{t-1} + Qz_t$$

$$y_t = Rx_{t-1} + Sz_t$$

- Note that here  $C$  is of full rank and has a well defined inverse  $C^{-1}$
- The solutions can be found from

$$\begin{aligned} 0 &= (F - JC^{-1}A)P^2 - (JC^{-1}B - G + KC^{-1}A)P - KC^{-1}B + H \\ R &= -C^{-1}(AP + B), \end{aligned}$$

$$\begin{aligned} &(N' \otimes (F - JC^{-1}A) + I_k \otimes (JR + FP + G - KC^{-1}A)) \text{vec}(Q) \\ &= \text{vec}(JC^{-1}D - L)N + KC^{-1}D - M \end{aligned}$$

and

$$S = -C^{-1}(AQ + D)$$

Explaining the solution

- We look for the laws of motion of the model

$$x_t = Px_{t-1} + Qz_t,$$

$$y_t = Rx_{t-1} + Sz_t.$$

- We begin by substituting the laws of motion into the two equations of the model
- Reduce each equation to one in which there are only two variables:

$$x_{t-1} \text{ and } z_t.$$

- Use the stochastic process in the expectational equation to replace

$$z_{t+1} = Nz_t + \varepsilon_{t+1}$$

- Taking expectations, the  $\varepsilon_{t+1} = 0$  disappear

Explaining the solution

- Begin with the model

$$\begin{aligned} 0 &= Ax_t + Bx_{t-1} + Cy_t + Dz_t \\ 0 &= E_t [Fx_{t+1} + Gx_t + Hx_{t-1} + Jy_{t+1} + Ky_t + Lz_{t+1} + Mz_t] \end{aligned}$$

- Substitute in

$$\begin{aligned} x_t &= Px_{t-1} + Qz_t, \\ y_t &= Rx_{t-1} + Sz_t. \end{aligned}$$

- In the first equation this gives

$$0 = A [Px_{t-1} + Qz_t] + Bx_{t-1} + C [Rx_{t-1} + Sz_t] + Dz_t$$

Explaining the solution

- In the second equation

$$\begin{aligned} 0 &= E_t [F [Px_t + Qz_{t+1}] + G [Px_{t-1} + Qz_t] + Hx_{t-1} \\ &\quad + J [Rx_t + Sz_{t+1}] + K [Rx_{t-1} + Sz_t] + Lz_{t+1} + Mz_t] \end{aligned}$$

- Substitute one more time in the second equation

$$\begin{aligned} 0 &= E_t [F [P [Px_{t-1} + Qz_t] + Q [Nz_t + \varepsilon_{t+1}]] + G [Px_{t-1} + Qz_t] \\ &\quad + Hx_{t-1} + J [R [Px_{t-1} + Qz_t] + S [Nz_t + \varepsilon_{t+1}]] \\ &\quad + K [Rx_{t-1} + Sz_t] + L [Nz_t + \varepsilon_{t+1}] + Mz_t] \end{aligned}$$

- This simplifies to (because  $E_t \varepsilon_{t+1} = 0$ ) and we remove the expectations operator

$$\begin{aligned} 0 &= F [P [Px_{t-1} + Qz_t] + QNz_t] + G [Px_{t-1} + Qz_t] \\ &\quad + Hx_{t-1} + J [R [Px_{t-1} + Qz_t] + SNz_t] \\ &\quad + K [Rx_{t-1} + Sz_t] + LNz_t + Mz_t \end{aligned}$$

Explaining the solution

- The two equations can be rearranged to give

$$0 = [AP + B + CR]x_{t-1} + [AQ + CS + D]z_t,$$

and

$$0 = [FPP + GP + H + JRP + KR]x_{t-1} \\ + [FPQ + FQN + GQ + JRQ + JSN + KS + LN + M]z_t.$$

- Since these equations need to hold for all  $x_{t-1}$  and  $z_t$ , it must be that

$$\begin{aligned} 0 &= AP + B + CR \\ 0 &= AQ + CS + D \\ 0 &= FPP + GP + H + JRP + KR \\ 0 &= FPQ + FQN + GQ + JRQ + JSN + KS + LN + M \end{aligned}$$

Explaining the solution

- The third equation is

$$0 = FP^2 + GP + JRP + H + KR$$

and the first is (if the inverse of  $C$  exists)

$$R = -C^{-1}AP - C^{-1}B$$

- Combining these one gets

$$\begin{aligned} 0 &= FP^2 + GP - J[C^{-1}AP + C^{-1}B]P \\ &\quad + H - K[C^{-1}AP + C^{-1}B] \\ 0 &= FP^2 - JC^{-1}AP^2 + GP - JC^{-1}AP^2 - JC^{-1}BP \\ &\quad + H - KC^{-1}AP - KC^{-1}B \\ 0 &= [F - JC^{-1}A]P^2 - [JC^{-1}B + KC^{-1}A - G]P \\ &\quad - KC^{-1}B + H \end{aligned}$$

Explaining the solution

- Here  $F$  is a  $1 \times 1$  matrix (a scalar)
- Finding the solution to the quadratic equation

$$0 = [F - JC^{-1}A]P^2 - [JC^{-1}B + KC^{-1}A - G]P \\ - KC^{-1}B + H$$

can be done using

$$0 = aP^2 + bP + c$$

- The solution to this equation is found from

$$P = \frac{-b \pm \sqrt{b^2 - 4ac}}{2a}$$

- There are usually two different solutions to this problem. We use  $|P| < 1$  in order to choose the stable root.
- Once  $P$  is known, finding  $R$  is simple using

$$R = -C^{-1}AP - C^{-1}B$$

Explaining the solution

- Finding  $Q$  (with  $P$  and  $R$  already known, from above)
- Use the equations

$$0 = FPQ + FQN + GQ + JRQ + JSN + KS + LN + M$$

and

$$0 = AQ + CS + D$$

- $S$  can be written as

$$S = -C^{-1}AQ - C^{-1}D$$

- Substitute this into the first equation

$$\begin{aligned} 0 &= FPQ + FQN + GQ + JRQ - JC^{-1}AQN - JC^{-1}DN \\ &\quad - KC^{-1}AQ - KC^{-1}D + LN + M \end{aligned}$$

- Rearrange to get

$$\begin{aligned} &[FP + G + JR - KC^{-1}A] Q + [F - JC^{-1}A] QN \\ &= JC^{-1}DN + KC^{-1}D - LN + M \end{aligned}$$

Explaining the solution

- This equation

$$\begin{aligned} &[FP + G + JR - KC^{-1}A] Q + [F - JC^{-1}A] QN \\ &= JC^{-1}DN + KC^{-1}D - LN + M \end{aligned}$$

has  $Q$  in two different places on the left hand side

- $Q$  in the final position in  $[FP + G + JR - KC^{-1}A] Q$
- $Q$  in the second to the last position in  $[F - JC^{-1}A] QN$

- Need to use a theorem from advanced matrix algebra

**Theorem 1** Let  $\mathbf{A}$ ,  $\mathbf{B}$ , and  $\mathbf{C}$  be matrices whose dimensions are such that the product  $\mathbf{ABC}$  exists. Then

$$\text{vec}(\mathbf{ABC}) = (\mathbf{C}' \otimes \mathbf{A}) \cdot \text{vec}(\mathbf{B})$$

where the symbol  $\otimes$  denotes the Kronecker product.

Explaining the solution

- Think of

$$\begin{aligned} & [FP + G + JR - KC^{-1}A]Q + [F - JC^{-1}A]QN \\ = & JC^{-1}DN + KC^{-1}D - LN + M \end{aligned}$$

as

$$WQI + XQN = Z$$

(notice that we added  $I$ ) where

$$\begin{aligned} W &= FP + G + JR - KC^{-1}A \\ X &= F - JC^{-1}A \\ Z &= JC^{-1}DN + KC^{-1}D - LN + M \end{aligned}$$

- Take  $\text{vec}$  of both sides of the equation, so

$$\text{vec}(WQI) + \text{vec}(XQN) = \text{vec}(Z)$$

- This equals

$$(I' \otimes W) \text{vec}(Q) + (N' \otimes X) \text{vec}(Q) = \text{vec}(Z)$$

or

$$(I' \otimes W + N' \otimes X) \text{vec}(Q) = \text{vec}(Z)$$

- If  $(I' \otimes W + N' \otimes X)$  is invertible

$$\text{vec}(Q) = (I' \otimes W + N' \otimes X)^{-1} \text{vec}(Z)$$

Explaining the solution

- What are  $\text{vec}$  and  $\otimes$  (the Kronecker product)

- First  $vec$

$$vec \left( \begin{bmatrix} a_{11} & a_{12} & a_{13} \\ a_{21} & a_{22} & a_{23} \end{bmatrix} \right) = \begin{bmatrix} a_{11} \\ a_{21} \\ a_{12} \\ a_{22} \\ a_{13} \\ a_{23} \end{bmatrix}.$$

- the columns are made into a vector

Explaining the solution

- The Kronecker product is

$$\begin{aligned} \mathbf{A} \otimes \mathbf{B} &= \begin{bmatrix} a_{11} & a_{12} \\ a_{21} & a_{22} \end{bmatrix} \otimes \begin{bmatrix} b_{11} & b_{12} \\ b_{21} & b_{22} \\ b_{31} & b_{32} \end{bmatrix} = \begin{bmatrix} a_{11}\mathbf{B} & a_{12}\mathbf{B} \\ a_{21}\mathbf{B} & a_{22}\mathbf{B} \end{bmatrix} \\ &= \begin{bmatrix} a_{11}b_{11} & a_{11}b_{12} & a_{12}b_{11} & a_{12}b_{12} \\ a_{11}b_{21} & a_{11}b_{22} & a_{12}b_{21} & a_{12}b_{22} \\ a_{11}b_{31} & a_{11}b_{32} & a_{12}b_{31} & a_{12}b_{32} \\ a_{21}b_{11} & a_{21}b_{12} & a_{22}b_{11} & a_{22}b_{12} \\ a_{21}b_{21} & a_{21}b_{22} & a_{22}b_{21} & a_{22}b_{22} \\ a_{21}b_{31} & a_{21}b_{32} & a_{22}b_{31} & a_{22}b_{32} \end{bmatrix}. \end{aligned}$$

Calibration

- Solution to model is numerical
- Need values for parameters
- Some we borrow from literature (quarterly)

- $\beta = .99$
- $\delta = .025$
- $\theta = .36$

- Need a value for  $A$

- Choose  $A$  so that  $\bar{H} = 1/3$
- Use stationary state equation for  $\bar{H}$

$$\bar{H} = \frac{1}{1 + \frac{A}{(1-\theta)} \left[ 1 - \frac{\beta\delta\theta}{1-\beta(1-\delta)} \right]}$$

- $A = 1.72$  for  $\bar{H} = .3335$

- $\bar{K} = 12.6695$  and using the production function,  $\bar{Y} = 1.2353$

- $\bar{r} = 1/\beta = 1.0101$
- From data for US use  $\gamma = .95$

Matices for Calibrated model

$$A = \begin{bmatrix} 0 \\ -12.670 \\ 0 \\ 0 \end{bmatrix} \quad B = \begin{bmatrix} 0 \\ 12.353 \\ 0.36 \\ -1 \end{bmatrix}$$

$$C = \begin{bmatrix} 1 & -1 & -1.5004 & 0 \\ 1.2353 & -0.9186 & 0 & 0 \\ -1 & 0 & .64 & 0 \\ 1 & 0 & 0 & -1 \end{bmatrix}$$

$$D = \begin{bmatrix} 0 \\ 0 \\ 1 \\ 0 \end{bmatrix}$$

Matices for Calibrated model

$$F = [0]$$

$$G = [0]$$

$$H = [0]$$

$$J = [ 0 \quad -1 \quad 0 \quad .0348 ]$$

$$K = [ 0 \quad 1 \quad 0 \quad 0 ]$$

$$L = [0]$$

$$M = [0]$$

$$N = [.95]$$

Numerical solution for model

- The quadratic equation gives the solutions

$$P = 1.0592 \quad \text{and} \quad P = 0.9537$$

- The stable value is

$$P = 0.9537$$

- The value for  $Q$  is

$$Q = 0.1132$$



- The matrices  $R$  and  $S$  are

$$R = \begin{bmatrix} 0.2045 \\ 0.5691 \\ -0.243 \\ -0.7955 \end{bmatrix} \quad \text{and} \quad S = \begin{bmatrix} 1.4523 \\ 0.392 \\ 0.7067 \\ 1.4523 \end{bmatrix}$$

Numerical solution for model

- The laws of motion are

$$\begin{aligned} \tilde{K}_{t+1} &= 0.9537\tilde{K}_t + 0.1132\tilde{\lambda}_t, \\ \tilde{Y}_t &= 0.2045\tilde{K}_t + 1.4523\tilde{\lambda}_t, \\ \tilde{C}_t &= 0.5691\tilde{K}_t + 0.3920\tilde{\lambda}_t, \\ \tilde{H}_t &= -0.2430\tilde{K}_t + 0.7067\tilde{\lambda}_t, \\ \tilde{r}_t &= -0.7955\tilde{K}_t + 1.4523\tilde{\lambda}_t. \end{aligned}$$

- Recall that  $\tilde{\lambda}_t$  follows the process

$$\tilde{\lambda}_t = .95\tilde{\lambda}_{t-1} + \mu_t$$

Two ways of finding the variances of the variables of the model

- Simulations
  - Run lots of simulated economies
  - Calculate the variances from this "data"
- Calculate variances from laws of motion
  - See book for details
- Need to calibrate  $var(\mu_t)$  so that  $var(\tilde{Y}_t) = 1.76\%$ 
  - gets standard error of  $\mu_t = .0032$

Tables of second moments

- Standard errors as fraction of output

	$\tilde{Y}_t$	$\tilde{C}_t$	$\tilde{H}_t$	$\tilde{r}_t$	$\tilde{I}_t$
<i>Standard error</i>	$5.484\sigma_\varepsilon$	$4.065\sigma_\varepsilon$	$1.640\sigma_\varepsilon$	$3.492\sigma_\varepsilon$	$11.742\sigma_\varepsilon$
<i>As % of output</i>	100%	74.12%	29.90%	63.67%	214.1%

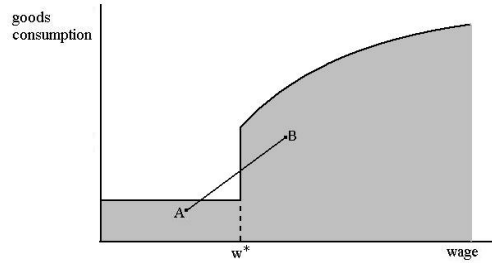
- Standard errors from the data

	$\tilde{Y}_t$	$\tilde{C}_t$	$\tilde{H}_t$	$\tilde{I}_t$
<i>As % of output</i>	100%	73.30%	94.32%	488.64%

- Does well for consumption
- Badly for hours worked and investment

```
% stationary state values are found in another program
A=[0 -kbar 0 0]';
B=[0 (1-delta)*kbar theta -1]';
C=[1 -1 -1/(1-hbar) 0
   ybar -cbar 0 0
   -1 0 1-theta 0
   1 0 0 -1];
D=[0 0 1 0]';
F=[0];
G=F;
H=F;
J=[0 -1 0 beta*rbar];
K=[0 1 0 0];
L=F;
M=F;
N=[.95];
Cinv=inv(C);
a=F-J*Cinv*A;
b=-(J*Cinv*B-G+K*Cinv*A);
c=-K*Cinv*B+H;
P1=(-b+sqrt(b^2-4*a*c))/(2*a);
P2=(-b-sqrt(b^2-4*a*c))/(2*a);
if abs(P1)<1
    P=P1;
else
    P=P2;
end
R=-Cinv*(A*P+B);
Q=(J*Cinv*D-L)*N+K*Cinv*D-M;
QD=kron(N', (F-J*Cinv*A))+(J*R+F*P+G-K*Cinv*A);
Q=Q/QD;
S=-Cinv*(A*Q+D);
Hansen's model with indivisible labor
```

- Objective: increase variance of hours worked
- Make labor indivisible
  - one works X hours per week or not at all
- Add unemployment
  - since some fraction of the population will not be working



Problem of non-convexity of consumption set

- In general, maximization is only valid over convex sets
- Def of a convex set
  - straight lines between any two points in set are also in set
- Example of a non-convex set

How non-convexity is fixed in Hansen's model

- The problem is the jump in income
  - between working and not working
- Hansen invented an "unemployment insurance"
- Lump sum transfers that make income equal for all
  - solves non-convexity problem
  - consumption increases smoothly with wage
  - since all receive same income (based on wages)
  - solve problem of too much heterogeneity

Household problem

- maximize

$$\max \sum_{t=0}^{\infty} \beta^t u(c_t, \alpha_t)$$

subject to

$$c_t + i_t = w_t h_t + r_t k_t$$

$\alpha_t$  = probability in time  $t$  of supplying  $h_0$  units of labor

- Expected utility

$$u(c_t, \alpha_t) = \ln c_t + h_t \frac{A \ln(1 - h_0)}{h_0} + A \left(1 - \frac{h_t}{h_0}\right) \ln(1)$$

$$u(c_t, \alpha_t) = \ln c_t + h_t \frac{A \ln(1 - h_0)}{h_0}$$

Household problem

- Maximization problem becomes

$$\max \sum_{t=0}^{\infty} \beta^t [\ln c_t + B h_t]$$

with

$$B = \frac{A \ln(1 - h_0)}{h_0}$$

- subject to constraints

$$\lambda_t k_t^\theta h_t^{1-\theta} = c_t + k_{t+1} - (1 - \delta)k_t$$

and

$$\ln \lambda_{t+1} = \gamma \ln \lambda_t + \varepsilon_{t+1}$$

Household problem

- First order conditions

$$0 = \frac{1}{c_t} \left( (1 - \theta) \lambda_t k_t^\theta h_t^{-\theta} \right) + B,$$

$$0 = -\frac{1}{c_t} + E_t \left[ \frac{1}{c_{t+1}} \theta \lambda_{t+1} k_t^{\theta-1} h_t^{1-\theta} + (1 - \delta) \right]$$

- With equilibrium condition, these simplify to

$$1 = \beta E_t \left[ \frac{C_t}{C_{t+1}} (r_{t+1} + (1 - \delta)) \right],$$

$$C_t = -\frac{(1 - \theta) Y_t}{B H_t}.$$

Full model

$$1 = \beta E_t \left[ \frac{C_t}{C_{t+1}} (r_{t+1} + (1 - \delta)) \right]$$

$$C_t = -\frac{(1 - \theta) Y_t}{B H_t}$$

$$\begin{aligned}
C_t + K_{t+1} &= Y_t + (1 - \delta)K_t \\
r_t &= \theta \lambda_t K_t^{\theta-1} H_t^{1-\theta} \\
Y_t &= \lambda_t K_t^\theta H_t^{1-\theta}
\end{aligned}$$

Stationary state

- Equations

$$\begin{aligned}
\frac{1}{\beta} &= \bar{r} + (1 - \delta) \\
\bar{C} &= -\frac{(1 - \theta)\bar{Y}}{B\bar{H}} \\
\bar{r} &= \theta \bar{K}^{\theta-1} \bar{H}^{1-\theta} \\
\bar{Y} &= \bar{K}^\theta \bar{H}^{1-\theta} \\
\bar{C} &= \bar{Y} - \delta \bar{K}
\end{aligned}$$

- solve to give

$$\bar{H} = -\frac{(1 - \theta)}{B \left(1 - \frac{\delta\theta\beta}{1-\beta(1-\delta)}\right)} \quad \text{and} \quad \bar{K} = \left[ \frac{\theta\beta}{1 + \beta(1 - \delta)} \right]^{\frac{1}{1-\theta}} \bar{H}$$

Stationary state

Comparing to basic Hansen model

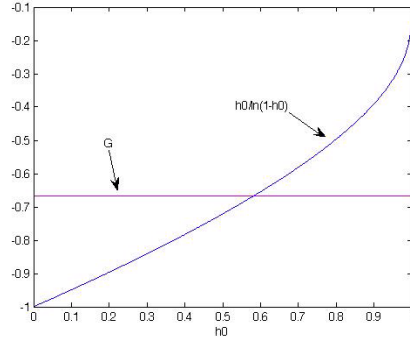
- To get same stationary state, need  $\bar{H}$  the same in both cases
- Then other variables will be the same
- Old stationary state equation

$$\bar{H} = \frac{1}{1 + \frac{A}{(1-\theta)} \left[1 - \frac{\beta\delta\theta}{1-\beta(1-\delta)}\right]}$$

- Set the two equal

$$\frac{1}{1 + \frac{A}{(1-\theta)} \left[1 - \frac{\beta\delta\theta}{1-\beta(1-\delta)}\right]} = -\frac{(1 - \theta)}{\frac{A \ln(1-h_0)}{h_0} \left(1 - \frac{\delta\theta\beta}{1-\beta(1-\delta)}\right)},$$

- We replaced  $B$  with  $\frac{A \ln(1-h_0)}{h_0}$
- Need to determine  $h_0$  that make the two SS the same



Stationary state

- Solve to get

$$\frac{h_0}{\ln(1-h_0)} = -\frac{\frac{A}{(1-\theta)} \left[ 1 - \frac{\beta\delta\theta}{1-\beta(1-\delta)} \right]}{1 + \frac{A}{(1-\theta)} \left[ 1 - \frac{\beta\delta\theta}{1-\beta(1-\delta)} \right]} = G$$

- G is a constant
- To find  $h_0$
- Get  $h_0 = .583$ ,  $\bar{\alpha} = .573$ , and  $\bar{H} = .3335$

Log-linear model

- Taking the log-linear approximation of the model gives

$$\begin{aligned} 0 &\approx \tilde{C}_t - E_t \tilde{C}_{t+1} + \beta \bar{r} E_t \tilde{r}_{t+1} \\ 0 &\approx \tilde{C}_t + \tilde{H}_t - \tilde{Y}_t \\ 0 &\approx \bar{Y} \tilde{Y}_t - \bar{C} \tilde{C}_t + (1-\delta) \bar{K} \tilde{K}_t - \bar{K} \tilde{K}_{t+1} \\ 0 &\approx \tilde{Y}_t - \tilde{\lambda}_t - \theta \tilde{K}_t - (1-\theta) \tilde{H}_t \\ 0 &\approx \tilde{Y}_t - \tilde{K}_t - \tilde{r}_t \end{aligned}$$

Solution method

- Use Uhlig's method

$$\begin{aligned} 0 &= Ax_t + Bx_{t-1} + Cy_t + Dz_t, \\ 0 &= E_t [Fx_{t+1} + Gx_t + Hx_{t-1} + Jy_{t+1} + Ky_t + Lz_{t+1} + Mz_t], \\ z_{t+1} &= Nz_t + \varepsilon_{t+1}, \quad E_t(\varepsilon_{t+1}) = 0, \end{aligned}$$

$$\text{where, } x_t = \begin{bmatrix} \tilde{K}_t \end{bmatrix}, y_t = \begin{bmatrix} \tilde{Y}_t, \tilde{C}_t, \tilde{H}_t, \tilde{r}_t \end{bmatrix}', \text{ and } z_t = \begin{bmatrix} \tilde{\lambda}_t \end{bmatrix}$$

- Solve for

$$\begin{aligned}x_t &= Px_{t-1} + Qz_t \\y_t &= Rx_{t-1} + Sz_t\end{aligned}$$

$$\begin{aligned}A &= \begin{bmatrix} 0 \\ -K \\ 0 \\ 0 \end{bmatrix} & B &= \begin{bmatrix} 0 \\ K(-\delta + 1) \\ \theta \\ -1 \end{bmatrix} \\C &= \begin{bmatrix} 1 & -1 & -1 & 0 \\ \bar{Y} & -\bar{C} & 0 & 0 \\ -1 & 0 & (1-\theta) & 0 \\ 1 & 0 & 0 & -1 \end{bmatrix} & D &= \begin{bmatrix} 0 \\ 0 \\ 1 \\ 0 \end{bmatrix} \\F &= [0], \quad G = [0], \quad H = [0] \\J &= [0 \quad -1 \quad 0 \quad \beta\bar{r}] & K &= [0 \quad 1 \quad 0 \quad 0] \\L &= [0], \quad M = [0], \quad \text{and } N = [\gamma].\end{aligned}$$

Results

- The linear policy functions are

$$\tilde{K}_{t+1} = .9418\tilde{K}_t + .1552\lambda_t$$

and

$$y_t = R\tilde{K}_t + S\lambda_t$$

where

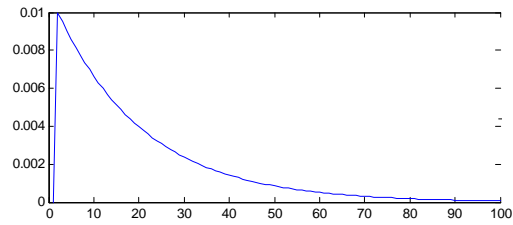
$$R = \begin{bmatrix} 0.055 \\ 0.5316 \\ -0.4766 \\ -0.945 \end{bmatrix} \quad S = \begin{bmatrix} 1.9418 \\ 0.4703 \\ 1.4715 \\ 1.9417 \end{bmatrix}$$

Results

- Using this model, we calculate the variances of the variables

	$\tilde{Y}_t$	$\tilde{C}_t$	$\tilde{H}_t$	$\tilde{r}_t$	$\tilde{I}_t$
<i>Standard errors</i>	$6.431\sigma_\varepsilon$	$4.081\sigma_\varepsilon$	$3.444\sigma_\varepsilon$	$4.514\sigma_\varepsilon$	$15.722\sigma_\varepsilon$
<i>As % of output</i>	100%	63.46%	53.55%	70.19%	244.5%

- Increased variance in hours worked
- Slight increase in investment
- Lower variance in consumption (compared to data)



Impulse response functions

- How does the economy respond to a one time shock to technology
- $\varepsilon_t = 0$  except  $\varepsilon_2 = .01$  Recall that  $\gamma = .95$

$$\tilde{\lambda}_t = \gamma \tilde{\lambda}_{t-1} + \varepsilon_t$$

- Response of technology (path of  $\tilde{\lambda}_t$ )

Impulse response functions

- Then calculate the time path of capital with  $\tilde{K}_1 = 0$  using

$$\tilde{K}_{t+1} = P\tilde{K}_t + Q\tilde{\lambda}_t$$

- get path of  $\tilde{K}_t$ . Use this to find path of other variables using

$$y_t = R\tilde{K}_t + S\lambda_t$$

Impulse response functions: Basic Hansen model

Impulse response functions: Hansen with indivisible labor

Comparing impulse responses

- Both models get same impulse
- Put each set of responses on different axis
- Get

Comparing impulse response

- Rotating so that we don't see the time axis



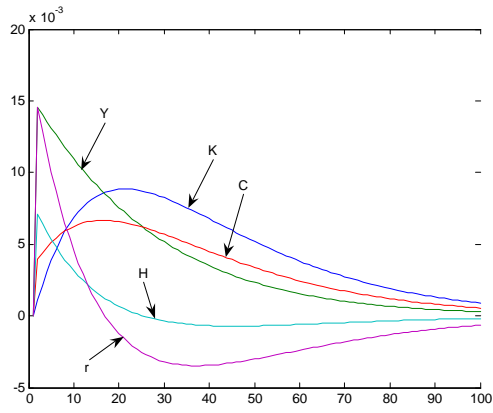


Figure 1: Responses of Hansen's basic model

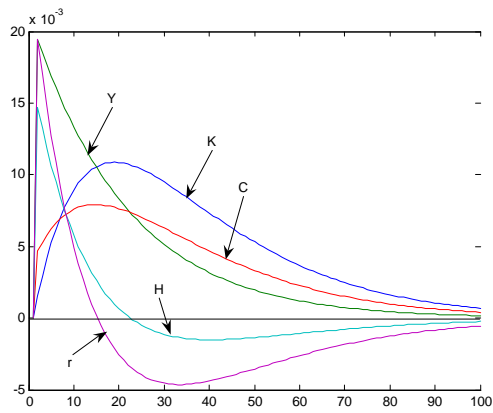


Figure 2: Responses for Hansen's model with indivisible labor

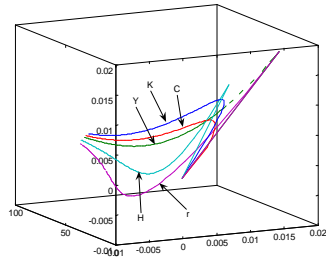


Figure 3: Responses for both Hansen models

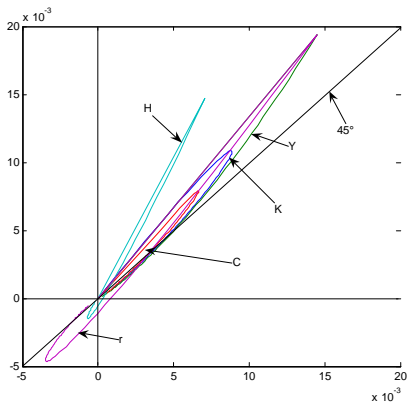


Figure 4: Comparing the response of the two models